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Wall Dynamics Tutorial

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 - **Consequence Analysis**
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The purpose of this presentation is to address the following topics

- Evaluation of vessel and piping wall temperatures using the fundamental heat transfer equation outlined in API Standard 521
- Advantages and characteristics of the wall segmentation approach implemented in Process Safety Office[®] SuperChems[™]
- Application of the wall dynamics approach in SuperChems[™] via 2 case studies
 - Case 1 Pressure Vessel
 - Case 2 Low-pressure Atmospheric Tank





A typical scenario that is almost always considered is the exposure of an equipment to a flame jet or pool fire

- Process vessels and piping components may fail because of excessive deviations in internal or external pressure, and/or wall temperatures
 - Equipment wall temperature increases
 - Yield and tensile strength of the vessel walls decrease
 - Resistance to internal pressure decreases while pressure vessel increases





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The fundamental heat transfer equation outlined in API Standard 521 is the basis for the wall dynamics approach

 $q_{absorbed} = \sigma(\alpha_{surface} \times \varepsilon_{fire} \times T_{fire}^4 - \varepsilon_{surface} \times T_{surface}^4) + h(T_{gas} - T_{surface})$

- \checkmark $q_{absorbed}$ is the absorbed heat flux from the fire, in W/m²
- \checkmark σ is the Stefan-Boltzman constant, which is 5.67x10⁻⁸ W/m²K⁴
- \checkmark $\alpha_{surface}$ is the equipment absorptivity, dimensionless
- \checkmark ε_{fire} is the fire emissivity, dimensionless
- \checkmark T_{fire} is the fire temperature, in K
- \checkmark $\varepsilon_{surface}$ is the equipment emissivity, dimensionless
- \checkmark $T_{surface}$ is the equipment temperature, in K
- h is the convection heat transfer coefficient of air/fire in contact with the equipment, in W/m^2K
- $rac{T_{aas}}$ is the temperature of air/fire in contact with the equipment surface, in K



API Standard 521 provides recommended values for jet fires when data is not available

Parameter	Description	Surface Average Heat Flux			
Leak rates		>2 kg/s	$\leq 2 \text{ kg/s}$		
		(Large Jet)	(Small Jet)		
$\varepsilon_{\rm f}$	Flame emissivity	0.33	NA		
$\mathcal{E}_{\mathbf{W}}$	Wall emissivity	0.75	NA		
$\alpha_{\rm w}$	Wall absorptivity	0.75	NA		
b	Convective heat transfer coefficient between equipment and surrounding air	40 W/m ² K	NA		
$T_{\rm g}$	Temperature of combustion gases flowing over the surface	1,173 K (900°C)	NA		
$T_{\rm f}$	Fire temperature	1,373 K (1,100°C)	NA		
$q_{ m f}$	Fire heat flux	100 kW/m^2	NA		
$q_{ m w}$	Absorbed heat flux	85 kW/m2	NA		

Flame Jet

Local Peak Heat Flux						
>2 kg/s	$\leq 2 \text{ kg/s}$					
(Large Jet)	(Small Jet)					
0.87	0.75					
0.75	0.75					
0.75	0.75					
$100 \text{ W/m}^2 \text{ K}$	$90 \text{ W/m}^2 \text{ K}$					

1,473 K (1,200°C)

1,373 K (1,100°C)

1,473 K (1,200°C) 350 kW/m^2 290 kW/m^2

1,373 K (1,100°C) 250 kW/m^2 210 kW/m^2



API Standard 521 also provides recommended values for open pool fires when data is not available

		Pool Fi	ire
Parameter	Description	Surface Average Heat Flux	Local Peak Heat Flux
ε _f	Flame emissivity	0.75	0.75
$\varepsilon_{\rm w}$	Equipment emissivity	0.75	0.75
α_{w}	Equipment absorptivity	0.75	0.75
b	Convective heat transfer coefficient between equipment and surrounding air	20 W/m ² K	20 W/m ² K
$T_{ m g}$	Temperature of combustion gases flowing over the surface	873 K (600°C)	1,323 K (1,050°C)
$T_{\rm f}$	Fire temperature	1,023 K (750°C)	1,323 K (1,050°C)
$q_{\rm f}$	Fire heat flux	60 kW/m^2	150 kW/m^2
$q_{\rm w}$	Absorbed heat flux	45 kW/m2	120 kW/m^2



Heat transfer is calculated as a function of time and includes several options

Heat transfer phenomena is calculated as a function of time

- From ambient to/from wall segment
- From wall segment to wall segment
- From wall segment to/from fluid
- Ambient to wall segment heat transfer options include insulation, solar heating, rain, water sprays, pool fires and jet fires
- Wall segment to fluid heat transfer include radiation, natural convection, forced convection, film boiling and pool boiling



A unique aspect of SuperChems[™] is how a vessel is sliced into segments

- No limit to the number of segments that the user can define
- Allows modeling flame jet impingement, and/or the effect of an open pool fire in different vessel sections / segments
- Ability to represent a wide variety of vessel shapes and heads, including composite vessels

Zone 1 Zone 2

Zone 3

Zone N-1 Zone N

Source: Melhem, G.A., Gaydos, D., 2014, "Properly Calculate Vessel and Piping Wall Temperatures During Depressuring and Relief", Process Safety Progress (Vol. 34, No.1)







Wall dynamics approach in SuperChems[™] is a very powerful tool

- Ability to predict the fluid dynamics of equipment containing liquids, vapors, and multiphase flows with or without chemical reactions
 - Including the Design Institute for Emergency Relief Systems (DIERS) technology to estimate vapor-liquid disengagement
- Ability to specify equipment internals using a variety of materials of construction
- Ability to connect multiple equipment and connect relief and process lines to the top and/or bottom of equipment
- Ability to include incoming and outgoing fluid streams





Vessel V-100 is protected by PRV-100 and exposure to an open pool fire has been identified as a contingency of concern

- Use of API Standard 521 recommended values for an open pool fire because no data is available on the pool fire characteristics
- The properties of the vessel and relief device under analysis are illustrated to the right
- SuperChems[™] new visual interface is used to model this system





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What are the necessary objects in SuperChems™?

- Under options, select the applicable "Study" Type"
 - For this type of analysis, select "Pressure" **Relief and Flare System**"
- Next, create 1 Scenario and name it appropriately
- 6 objects will appear under Case 1 scenario:
 - For this type of calculation, we only need the following objects: Mixture, Vessel, Piping Layout, and Pressure Relief Valve





Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

e	
re Relief and Flare System	Dynamic Flowsheet Simulation
quence Modeling	Quantitative Risk Analysis
e Modeling	

roup Meeting
ASE 1
Site DEFAULT
Mixture CASE 1
Vessel CASE 1
Top Primary Piping Layout CASE 1 - P
Stream [NO FLOW]
Project Data DEFAULT
Models (1)
ASE 1 - MITIGATION



How should a vessel be defined?

- Right click under "Vessel", select "New", and name the Vessel appropriately
 - ► Note that SuperChemsTM will automatically assign the new vessel to the scenario of interest
- Other options include:
 - Copy, Rename, Define, Change, Import
- A vessel can also be defined under "Define" tab at the top, and selecting "Equipment"





What are the necessary specifications?

CASE 1

- Design pressure
- Design Temperature
- Vessel Type
- Length
- **Inside Diameter**
- Shell Thickness
- Elevation
- Head Type
- Wall Thickness

CASE 1							
Specification Options	Report Comments Geometry	and Stress Toolbox					
Basic	CASE 1						
Notes Profile	Description	CASE 1 Vessel	P&IDs	NA			
Options External Fire	Location	NA	Equipment type	Vessel	*		
Heating and Cooling Water Spray	Manufacturer	NA	Vessel built per	ASME Section	VIII		
Insulation Internal	Serial number	NA	Applicable relief code	API 520/521	•		
Eductor	Pressure				C Temperature		
Calorimeter	Design pressure	300	psig		Design temperature	230] °C
	Vacuum pressure	-14.7	psig		Minimum temperature	-29] °C
	Normal operating pressure	200	psig		Normal operating temperature	75] °C
	Maximum pressure	200	psig		Maximum temperature	75] ° c
ĺ	Physical Dimensions		_		·		
	Vessel type	Vertical Cylindrical	Material of construction	STEEL	•		
	Length	30	ft Actual material	CARBON STE	EEL, C-Mn-Si		
	Inside diameter	15	ft Internals/User defined mass	0		в	
	Shell thickness	0.0417	ft Liquid pool bottom elevation	1		ft	
			Grade bottom elevation	1		ft	
	Head	Тор	Bottom				
	Туре	Elliptical 2:1	Elliptical 2:1		•		
	Wall thickness	0.0417	ft 0.0417		ft		

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation



Always check the vessel geometry under "Geometry and Stress" tab to ensure the vessel dimensions



Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

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Vessel specification tabs appear based on the options selected

To perform the wall dynamics, check "Enable Fire Loadin

CASE 1				
Specification Options	Report Comments Geometry and Stress Toolbo	ox		
Basic Notes	Enable Fire Loading			
Profile Options	Fire flux	29841.3037	W/m²	Fire Loading Methodology API-521 Fire Flux
External Fire Heating and Cooling	Fire start time	0	h	Wetted area fraction confined or indoors
Water Spray	Fire duration	4	h	Adequate drainage and fire fighting equipment are present
Insulation Internal	Fraction exposed to fire	0.6301]	✓ Adjust wetted area for liquid level
Eductor Calorimeter	Wetted area	111.3123	m²	Maximum liquid level 70 %
				Mitigation factor 1
				O API-2000 Fire Flux
				O NFPA-30/OSHA 1910
				O User-defined fire loading
	Options Remove bottom head from estimate of wetter Remove top head from estimate of wetted a	ed area irea		
	Description Area m	2		
	Allowance for relief and process piping 11.13			

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

	Specification Options Rep	ort Comments Geometry and Stress Toolbox
	Profile	✓ Insulation
a"	External Fire	Internal
9	Heating and Cooling	Eductor
	Vater Spray	 Calorimetry
	Options	



Apply the appropriate Carbon Steel Plate and Allowable Stress Curve

- Go to "Toolbox" tab, and click the icon "Vessel, Apply Carbon Steel Plates"
- SuperChems[™] has prepopulated several carbon steel plate and allowable stress curves
- In this example, SA-516 Grade 70 Carbon Steel is applied based on the vessel material of construction





Temperature and pressure ratings can be verified by switching to SuperChems[™] classic

Under "File" tab, click the "Classic" icon

Under the Vessel object, click the "Verify T&P Design Ratings" icon



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ioMosaic uses 2/3 of the Ultimate Tensile Strength (UTS) as a conservative limit based on NFPA 68 Section 5.3.3.1

Vessel Name	CASE 1							
Vessel Type	Vertical Cylind	rical; User de:	fined h	neads				
Vessel Top Head Type	Elliptical 2:1							
Vessel Bottom Head Type	Elliptical 2:1							
** METERIAL OF CONSTRUCTION SPECIFICATIONS. OBTAIN	THIS INFORMATION	FROM ASME TAE	LES					
Actual Material of Construction Description	CARBON STEEL, C-	-Mn-Si						
Databank material of construction used for thermal	STEEL	STEEL	-					
Specification	SA-516							
P-No, G-No, or S-No	P1, G2							
Product Form	Steel Plate or S	Sheet						
Grade	70							
Note 1	See Note 17 in A	ASME Boiler and	i Press	sure Vessel Co	de. Page 280			
Note 2	External pressur	re chart 5-UCS	-28.2					
Minimum Temperature. °C	-28.8	9						
Minimum yield strength. psia	38000.0	0						
Minimum tensile strength. psia	70000.0	0						
Allowable Stress Basis	ASME							
Temperature. °C	-28.8	9 34	3.33	371.11	398.89	426.67	454.44	482.
Allowable Stress. psia	1.750E+0	4 1.750	E+04	1.660E+04	1.480E+04	1.200E+04	9.300E+03	6.500E+
Young's Modulus of Elasticity. psia	3.410E+0	7 3.178	E+07	3.119E+07	3.054E+07	2.985E+07	2.911E+07	2.832E+
Coefficient of Linear Thermal Expansion. /°C	7.387E-0	6 1.507	E-05	1.590E-05	1.665E-05	1.733E-05	1.795E-05	1.850E-
Poisson's Ratio	0.29	0 0	.290	0.290	0.290	0.290	0.290	0.2
Failure Stress Basis	2/3 UTS							
Temperature. °C	-253.88	9 37	.778	93.333	148.889	204.444	260.000	315.5
Failure Stress. psia	46666.66	7 46666	.667	46666.667	46666.667	44151.697	41357.285	39121.7

6	38283.433	37724.551	37165.669	36327.345	35768.463	33253.493
6	343.333	371.111	398.889	426.667	454.444	482.222
0	0.290	0.290	0.290	0.290	0.290	0.290
5	1.876E-05	1.900E-05	1.922E-05	1.943E-05	1.963E-05	1.982E-05
7	2.791E+07	2.748E+07	2.704E+07	2.659E+07	2.613E+07	2.565E+07
3	4.500E+03	2.500E+03				
2	510.00	537.78				

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Defining a mixture object

Select the basis (Mass or Mole), and then add components by clicking the green button +

✓ Note that if the "Automatic BIPS Calculation" option is selected, SuperChems[™] will automatically apply the Binary Interaction Parameters (BIPS) for us

Basic Infomation										
Name CASE 1										
_										
Validation Check 🗸 🛛 Aut										

Kij	ETHANE	PROPANE	n-BUTANE	n-PENTANE
ETHANE	0	0.00137	0.00706	0.0072
PROPANE	0.00137	0	0.00142	0
n-BUTANE	0.00706	0.00142	0	0
n-PENTANE	0.0072	0	0	0
	010072	-	~	~
	0.0072	-	-	-
	0.0012		-	
	ETHANE	PROPANE	n-BUTANE	n-PENTANE
Lij	ETHANE 0	PROPANE -0.01489	n-BUTANE -0.02206	n-PENTANE 0.0016
Lij ETHANE PROPANE	ETHANE 0 0.01489	PROPANE -0.01489 0	n-BUTANE -0.02206 -0.03814	n-PENTANE 0.0016 0
Lij ETHANE PROPANE n-BUTANE	ETHANE 0 0.01489 0.02206	PROPANE -0.01489 0 0.03814	n-BUTANE -0.02206 -0.03814 0	n-PENTANE 0.0016 0



Always ensure the mixture Vapor-Liquid Equilibrium (VLE)





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Defining the piping layout and associated pressure relief device objects

- Click on "Settings" and a new window will pop up
- SuperChems[™] contains a database with thousands of relief valves to select from
- You can filter by Source, Manufacturer, Model, Orifice, or Flow Service

🕼 Import Relief I	Device								- 0	
Relief Devices: (10	87 found)									
Source 🔽	Manufacturers 🔲 NB-18									
Source	Manufacturer	Model	•	Туре	Inlet	Orifice	Outlet	Area	Flow Basis	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	1	F	2	0.307	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	1.5	н	2	0.785	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	1.5	Н	3	0.785	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	2	J	3	1.287	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	3	L	4	2.853	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	4	Ρ	6	6.38	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	6	R	8	16	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 243		р	8	Т	10	26	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 249		р	1	F	2	0.307	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 249		р	1.5	н	2	0.785	API	
Manufacturers	ANDERSON GREENWOOD	TYPE 249		р	1.5	н	3	0.785	API	
Manufacturore	ANDERSON GREENWOOD	TVDE 240		n .	2	1	2	1 207	۸DI	Ľ
ANDERSON GREEF Flow Service Device Certifica Device is C Device is C Device is C Device is A Device is A Device is A Device is A Device is A	Twophase Twophase Tion ertified for Gas Flow ertified for Iiquid Flow ertified for Steam Flow SME-SECTION I Certified SME-SECTION IV Certified SME-SECTION VIII Certified									
								אר	Cancel	

		OK	Cancel



In this example, an Anderson Greenwood 4P6 pilot pressure relief valve is selected

- SuperChems[™] populates
 almost all required fields
- You still need to specify the Set Pressure and Reseat Pressure

PRV Specifications Low Pressure Lift vs. Overpressure Lift vs. Backpressure SDOF Parameters Data Sheet Cd Calculator CASE 1 - P VALVE	
CASE 1 - P VALVE Description Anderson Greenwood Series 200/400/500/70 PRV numeric ID 0 Model number TYPE 243 Equipment protected Case 1 Service Gas Serial number NA Manufacturer ANDERSON GREENWOOD Design type Pilot Spring number NA Location P & ID Image: Service Design type Pilot Service Service	
DescriptionAnderson Greenwood Series 200/400/500/70PRV numeric ID0Model numberTYPE 243Equipment protectedCase 1ServiceGasSerial numberNAManufacturerANDERSON GREENWOODDesign typePilotSpring numberNALocationP & IDImage: ServiceSpring numberNa	
Equipment protected Case 1 Service Gas Serial number NA Manufacturer ANDERSON GREENWOOD Design type Pilot Image: Spring number NA Location P & ID Image: Spring number NA Image: Spring number NA	
Manufacturer ANDERSON GREENWOOD Design type Pilot Spring number NA Location P & ID Image: Comparison of the spring number Image:	
Location P & ID Parameters	
Associated RD	
Associated ND Discharge Location	
COutlet Flange	
Pressure rating 599.9977 psig Class ANSI Pressure rating 599.9977 psig Class ANSI	
Inlet Schedule Outlet Schedule	
Name Value Unit Name Value Unit	
Nominal pipe size 4 Nominal pipe size 6	
Piping schedule 40 Piping schedule 40	
Outside Diameter 0.5208 ft	
Wall Thickness 0.01975 ft Wall Thickness 0.02333 ft	
Flow Area 0.00821 m^2	
Pipe Info Pipe Info	
C Device Certification	
Certified for gas flow ASME-SECTION I certified Flow type Gas/Vapor Liquid Two phase	
Certified for liquid flow ASME-SECTION IV certified Discharge coefficient 0.975 0.62 0.85	
Certified for steam flow ASME-SECTION VIII certified	
Modulating valve Designated as spare Slip ratio multiplier	
c Lifting Characteristics Slip ratio exponent 0.0001	
Minimum lift 0.0083 ft Maximum lift 0.0333 ft	
Device has a restricted lift	
Restricted lift 0 ft 0.0594 ft	
Available flow area 0 %	
Flow area basis API Reset pressure 270 psig	
Maximum blowdown 10 % Actual blowdown 10 %	

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation



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In the Piping Layout object, select the applicable segments

- Adjust the elevation of the "1st segment relative to vessel bottom"
 - Account for the length of top / bottom heads
- For this dynamic evaluation, we will only use the pilot 4P6 valve

CASE 1 - P VALVE			
All Piping Units Piping Units Specifications Charts Toolbox			
Properties	CdL = 0.62, CdV = 0.975, Cd2P = 0.85		
Short description Case 1 - P Valve	CASE 1 - P VALVE Gas/vapor discharge coeffic	0.975	
PID/PFD reference NA	CASE 1 - P VALVE Liquid discharge coefficient	0.62	
Overall mass flow multiplier for flow dynamics	CASE 1 - P VALVE 2phase discharge coefficien	0.85	
1st segment elevation relative to vessel bottom 37.5 ft	Thermodynamic Flow Path		
Layout is an open relief path			
Layout is a header/network			
Use CCF	Nozzle Flow Method]
Use design/derated flow area for PRV	O Use dH		
	O Use VdP integral		
- Available Units	- Selected Units		
		1. D.VALVE	
		I - P VALVE	
Control Valve CV - XT 0.52			



Next, identify and apply the correct source term model for the simulation

- Right click in "Models"
- Select "Flow and Source Term"
- Select "Dynamic Vessels: Twophase"

1			
	-	🗐 Models (Elow and Source
		de Duosi	Flow and source
			Network Flow
	• =	CASE 1 - R	Control
		L	





In the dynamic vessels two-phase model, specify initial conditions and simulation parameters

- Fluid Phase = Saturated Liquid
- Pressure = 200 psig
- Under relief piping path, specify the backpressure (0 psig) and Flow Type (Vapor)
- Starting Time = 0 hours
- Final time = 4 hours, fire duration
- Select "External fire exposure" checkbox
- Select "Perform Detailed Vessel Wall Heat Transfer Dynamics" checkbox and select the number of segments (5 in this example)



To properly calculate the mass contents, go to "Toolbox" and click "Specify Fill Level"

- In this example, the normal liquid level is 70%
- Based on the initial pressure and mixture composition, SuperChems[™] will calculate the initial mass and starting temperature

👜 Dynamic Vessels: Two-phase		
Inputs Results Charts Toolbox	Notes Data Sets	
Delete Delete Model IO	Export Data Export Data for Group Reporting Specify Fill Leve	Level el Vary X to match T/P specs
Design a Cyclone Separator	Cyclone Results	
	🔝 Specify Fill Le	vel in Percent – X
	Fill Level 70	%
		OK Cancel

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

eset

set simulation startina



Pipe Wall Dynamics Pipe Wall Dynamics



Output Thinning Output Thinning



The screenshot below shows the initial conditions and parameters for the dynamic simulation

(tta) Dynamic Vessels: Two-phase			
Inputs Results Charts Toolbox Not	es Data Sets		
Cancel Update Run			
Specifications Connectivity Run Para	meters Stop Conditions Vesse	Wall Dynamics Accuracy	
Vessel Initial Conditions			
Total volume	46267.0912 gal	ſ	Fluid Phase
			O Saturated liquid
Available volume	46267.0912 gal		O Liquid full
Contents mass	135085.5188 Ib		O Vapor full
		Ľ	
Contents	Normal operating	Maximum operating Minimum o	design Maximum design
Temperature. C 75	/5	75 -29	230
Pressure. psig 200	200	-14./	300
Top: primary 0 Time Analysis Starting time	CASE 1 - P VALVE	/apor	Sir
Final time	4 h		
Continue from previous simulation	1		
 Advanced Options Perform Detailed Vessel Wall Automatically divide segment 	Heat Transfer Dynamics	Flowsheet Disable all incoming flow	Find Required Flow Area (
Number of vessel wall segments	5		
Specify mixture fractions			





Specify the vessel wall dynamics properties to use the fundamental heat transfer equation outlined in API Std 521

Ensure that the "Fire Exposure" option is checked



Input the correct parameters based on API Standard 521 7th edition for the "Fire/Flame Properties" and the "Wall Properties" sections

	- Fire/Flame Properties and Exposure Parame	tors	Wall Properties		-
	Fire start time	0 h	Material of construction description	CARBON STEEL, C-Mn-Si	
	Fire duration	4 h	Databank material of construction name	STEEL	
	Emissivity	0.75	Metal mass (Internals + User defined)	0 ІЬ	
	Flame temperature	1050 °C	Outer surface emissivity	0.75	
	Gas temperature	1050 °C	Inner surface emissivity	1	
	Convective heat transfer coefficient	20 W/m²/°C			
	Geometric view factor	1	Absorptivity	0.75	
l	Atmospheric transmissivity	1	Wall/Vapor heat transfer Coefficient	75 W/m²/°C Upper Limit	
	Match fire flux data specified in vessel obje	ect	Wall/Liquid heat transfer coefficient	2500 W/m²/°C Upper Limit	
	User defined fire flux	29841.3037 W/m ²	Wall/Condensing film heat transfer Coefficient	0 W/m²/°C Upper Limit	
	Calculated fire flux	118255.6595 W/m ²	l		



Define the properties for all the wall segments

Specify wall temperature equal to fluid starting temperature (75 °C) and check the applicable "Visible to fire" and "Engulfed by fire" checkboxes for all segments as applicable

				Wall Data Wall Segmentation			
Specifications Connectivity Run Parameters Stop (Conditions Vessel Wall Dynamics Accuracy			C Heat Transfer Segment			
Wall Data Wall Segmentation Heat Transfer Segment				Bottom Segment 0 -> 1	Site Ambient Temperature = 25 °C. Init	tial Vessel Contents Temperature = 7	75 °C
Bottom Segment 0 -> 1	Site Ambient Temperature = 25 °C. Initia	al Vessel Contents Temperature = 75 °C		Segment 1 -> 2	Top Segment 4 -> 5		
Segment 1 -> 2	c Bottom Segment 0 -> 1		,	Segment 2 -> 3	Visible to fire		
Segment 2 -> 3	Visible to fire			Top Segment 4 -> 5	Englufed by fire		
Top Segment 4 -> 5	Englufed by fire				Protected by water spray		
	Protected by water spray				Visible to solar heating		
	Visible to solar heating				Exposed to rain		
	Exposed to rain				Buried in semi-infinite material		
	Buried in semi-infinite material				Insulation layer thickness	0	ft
	Insulation layer thickness	0	ft		Initial insulation temperature	75	°C
	Initial insulation temperature	75	°C				
	leftel well been endered	75			Initial wall temperature	/5	°C
	Initial wall temperature	15			Maximum Do/t	212.6299	User override
	Maximum Do/t	212.6299	User override				
					Associated/Calculated Data		
	Associated/Calculated Data				Bottom segment elevation	31.1406	ft
1	·				Tax account elevation	27 5/17	
					Top segment elevation	57.3417	π

Specifications Connectivity Run Parameters Stop Conditions Vessel Wall Dynamics Accuracy



Click "Run" and wait for the dynamic simulation to finish

Inputs Results Charts Toolbox Notes Data Sets Summary Flows Profiles Detailed Profiles Composition Export Vessel Options & Considerations Vessel Connection Relief Piping Backpressure psig Flow type Vessel Options & Considerations Vessel Connection Relief Piping Backpressure psig Flow type Overall Balance Initial Final Final Initial Time h 0.0000 4.000 Time h 0.0000 4.000 4.000 Temperature *C 74.892 947.7 872.8 Pressure psig 200.0 271.3 71.327 71.327 Vapor volume gal 13,895 48,337 34,442 4.442 Liquid mass Ib 1.31732E+05 0.0000 -1.31732E+05 1.guid volume gal 32,372 Total mass Ib 1.35086E+05 4.921 -1.30164E+05 1.30164E+05	Pressure dP/dt Temperate
Inputs Kesuts Charts Toolbox Notes Data Sets Summary Flows Profiles Detailed Profiles Composition Export Relief Piping Secondary Piping Backpressure psig Flow type External fire exposure Vessel Connection Relief Piping Backpressure psig Flow type TOP: Primary Piping CASE 1 - P VALVE 0 Vapor Vapor Overall Balance Initial Final Final Final Final Initial Time h 0.0000	Pressure dP/dt Temperat
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Liquid volume gal 32,372 0.0000 -32,372	
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Total volume gal 46.267 48.337 2.070	
Volume Full of Liguid % 69.968 0.0000 -69.968	
Composition Balance	
laitial Liquid - Final Liquid - Initial Vanas - Final Vanas - Initial Tatal - Final Tatal - Change T	-t-l
Initial Liquid Final Liquid Initial Vapor Final Vapor Initial Iotal Final Iotal Change id	otai
ETHANE Ib 6,225 0.0000 763.5 79.491 6,989 79.491 -6,909	
PROPANE ID 19,478 0.0000 1,019 430.8 20,497 430.8 -20,066	
n-DOTAINE ID 59,055 0.0000 690.9 1,345 40,520 1,345 -39,183	
11 ENTRALE 10 00,004 0.0000 000.1 0,000 07,074 0,000 -04,000	
Totals 1.31732E+05 0.0000 3.353 4.921 1.35086E+05 4.921 -1.30164E	+05

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

daries —					
		Maximum	Time h	Point	
	psig	414.1	0.5020	173	1.38 x DESIGN P
	psig/h	1,904	0.0760	34	
re	°C	947.7	4.000	716	3.90 x DESIGN T
	°C/h	2,108	0.6200	287	
	lbf	3,163	0.5020	171	
g input	W	1.60372E+07	0.0000	0	



Under "Charts" tab, the user can illustrate several types of dynamic results such as pressure profile



Time h

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

Pressure psig

Pressure psig

ioMosaic[®]

The user can also illustrate other results such as venting history profile



Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

Total Mass Flow Rate lb/h Primary Piping Gas/Vapor Mass Flow Rate lb/h

Under "Wall Dynamics" tab, the user can illustrate wall segment temperature profiles

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- Wall Segment 0 1. Bottom
- Wall Segment 1 2
- Wall Segment 2 3
- Wall Segment 3 4
- ----- Wall Segment 4 5. Top
- Fluid Temperature. °C

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

Based on the wall failure stress profiles, V-100 stress exceeds 2/3 of the Ultimate Tensile Strength (UTS)

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

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- Wall Segment 0 1. Bottom. Failure Stress [2/3 UTS]
- Wall Segment 1 2. Failure Stress [2/3 UTS]
- Wall Segment 2 3. Failure Stress [2/3 UTS]
- Wall Segment 3 4. Failure Stress [2/3 UTS]
- Wall Segment 4 5. Top.
- Failure Stress [2/3 UTS]
- Wall Segment 0 1. Bottom. Actual Stress
- Wall Segment 1 2. Actual Stress
- Wall Segment 2 3. Actual
- Stress
- Wall Segment 3 4. Actual
- Stress
- Wall Segment 4 5. Top.
- Actual Stress

PRV-100 may not adequately protect V-100 in the event of exposure to an open pool fire

- The pressure relief system may be inadequate because the expected vessel pressure is above the Maximum Allowable Accumulated Pressure (MAAP = 1.21 x MAWP)
- Additionally, the vessel stress exceeded 2/3 of the UTS, so the equipment is expected to fail before 4 hours
- Next, we investigate the impact of installing a larger relief device (6R8)
- Note that valid mitigation solutions are typically the following:
 - Install fire-proof insulation
 - Replace the pressure relief valve for an emergency depressuring system
 - Use of water sprays

From the overpressure point of view, the system seems adequate because maximum pressure is below MAAP (1.21 x MAWP)

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— Pressure psig

However, V-100 is still expected to fail after 15 minutes of fire exposure because the vessel stress exceeds 2/3 of the UTS

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

© ioMosaic Corporation

- Wall Segment 0 1. Bottom. Failure Stress [2/3 UTS]
- Wall Segment 1 2. Failure Stress [2/3 UTS]
- Wall Segment 2 3. Failure Stress [2/3 UTS]
- Wall Segment 3 4. Failure Stress [2/3 UTS]

Wall Segment 4 - 5. Top. Failure Stress [2/3 UTS]

- Wall Segment 0 1. Bottom. Actual Stress
- Wall Segment 1 2. Actual
- Stress
- Wall Segment 2 3. Actual
- Stress
- Wall Segment 3 4. Actual
- Stress
- Wall Segment 4 5. Top.
- Actual Stress

Case Studies in SuperChems™ **Case 2 – Low-Pressure Atmospheric Tank**

Atmospheric Storage Tank T-100 has been identified to be exposed to thermal radiation due to a nearby pool fire

- A nearby loss of containment scenario results in leakage of a flammable material resulting in a pool fire
- Using SuperChems[™], it is estimated that T-100 is exposed to a heat flux of 25 kW/m² with a duration of 5 minutes
- The properties of the vessel under analysis are illustrated to the right

MAWP < 15 psig MAWT = 250 °C Length = 35 ft Diameter = 100 ft Bottom Head = Flat Top Head = Floating Roaf Shell Thickness = 0.5 in Thickness of Top/Bottom Heads = 0.5 in Material = SA 516-70 Pressure = 0 psig Temperature = 25 °C Liquid Level = 85% Molar Composition = 100% Decane

Floating Roof

T-100

API Standard 650 may be used to define the failure criterion for low-pressure atmospheric storage tanks

- The goal is to identify whether the mechanical integrity of the tank would be compromised, resulting in potential equipment failure
- Evaluation of T-100 mechanical integrity needs to account for the tank wall temperatures and heat radiation received
- Based on API Standard 650 12th Edition, the failure temperature of a carbon steel storage tank is indicated as 93 °C, and for well-maintained and inspected storage tanks, the failure temperature is indicated as 250 °C

The image below illustrates simulation initial conditions and parameters when tank T-100 is exposed to 25 kW/m²

(b) Dynamic Vessels: Two-phase	
Inputs Results Charts Toolbox Notes Data Sets	
Specifications Connectivity Run Parameters Stop Conditions Vessel Wall Dynamics Accuracy	
Vessel Initial Conditions	
Total volume 275085.707 ft ³	
O Saturated liquid	
Available volume O Liquid full	
Contents mass 10500000 Ib O Vapor full	
Contents Normal operating Maximum operating Minimum design Maximum design	
Temperature. °C 25 25 -29 230	
Pressure. psig 0 0 0 -14.7 14.7	
Relief Piping Path	
Flow path Backpressure. psig Piping connection Flow type	
PLOATING ROOF No flow	
C Time Analysis	
Starting time 0 min Check starting co	nditions only
▼ External fire expo	sure
Final time 60 min	
Continue from previous simulation	
Advanced Options	
Perform Detailed Vessel Wall Heat Transfer Dynamics Flowsheet Flowsheet	h an ideal nozzle
Disable all incoming flow	
✓ Automatically divide segments Disable all outgoing flow	
Number of vessel wall segments 20	
Specify mixture fractions	
C Mixture Composition	
Mass O Mole	
Compound Formula ID MW Mass Fraction Mole Fraction User Composition	
n-DECANE C10H22 9 142.285 0.9993 0.9965 0.9993	
NITROGEN N2 980 28.014 0.0007 0.0035 0.0007	

ioMosa

Wall dynamics parameters and properties are properly specified for this scenario

Vessel Initial Conditions			-					
 Solar heating Fire exposure 			Wa	all Data Wall Segmentation				
Water exposure is not turned on for ves	sel		C	Heat Transfer Segment				
Rain is not turned on for vessel				Bottom Segment 0 -> 1	Site Ambient Temperature = 25 °C. Init	ial Vessel Contents Temperature	= 25 °C	
			-	Segment 1 -> 2	c Bottom Segment 0 -> 1			
Fire/Flame Properties and Exposure Parameters			Segment 2 -> 3	Virible to fire				
Eire start time	0 min			Segment 3 -> 4				
The start time	<u> </u>			Segment 4 -> 5	Englufed by fire			
Fire duration	5 min			Segment 5 -> 6	Protected by water spray			
				Segment 6 -> 7				
Emissivity	0.75			Segment 7 -> 8	Visible to solar heating			
				Segment 9 -> 10	Exposed to rain			
Flame temperature	750 °C			Segment 10 -> 11	Buried in semi-infinite material			
				Segment 11 -> 12				
Gas temperature	600 °C			Segment 12 -> 13	Insulation layer thickness	0	ft	
	20			Segment 13 -> 14				
Convective heat transfer coefficient	20 W/m²/°C			Segment 14 -> 15	Initial insulation temperature	25	°C	
Geometric view factor	1			Segment 15 -> 16	laitial well to waters	25		
Geometric view factor				Segment 16 -> 17	initial wall temperature	23		
Atmospheric transmissivity	0.387			Segment 17 -> 18	Maximum Do/t	212.6299	User ov	verride
				Segment 18 -> 19				
Match fire flux data specified in vessel object			Top Segment 19 -> 20					
	25000				Associated/Calculated Data			
user defined fire flux	23000 W/m *				L			
Calculated fire flux	25026.1371 W/m ²							

Based on the dynamic simulations results, it can be observed that T-100 fluid temperature stays reasonably constant

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

— Temperature °C

Wall temperature profiles indicate that segments not covered by liquid get hotter sooner and then cool down after 5 minutes

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

- ----- Wall Segment 0 1. Bottom
- ---- Wall Segment 1 2
- Wall Segment 2 3
- Wall Segment 3 4
- Wall Segment 4 5
- Wall Segment 5 6
- Wall Segment 6 7
- Wall Segment 7 8
- ---- Wall Segment 8 9
- Wall Segment 9 10
- Wall Segment 10 11
- ---- Wall Segment 11 12
- Wall Segment 12 13
- Wall Segment 13 14
- ----- Wall Segment 14 15
- ----- Wall Segment 15 16
- ---- Wall Segment 16 17
- ---- Wall Segment 17 18
- ---- Wall Segment 18 19
- Wall Segment 19 20. Top
- Fluid Temperature. °C

T-100 mechanical integrity is not expected to be compromised based on the detailed wall dynamics results

Source: Process Safety Office[®] SuperChems[™] - ioMosaic Corporation

Wall Segment 1 - 2

Wall Segment 2 - 3

- Wall Segment 3 4
- ----- Wall Segment 4 5
- Wall Segment 5 6
- ---- Wall Segment 6 7
- Wall Segment 7 8
- Wall Segment 8 9
- Wall Segment 9 10
- Wall Segment 10 11
- Wall Segment 11 12
- Wall Segment 12 13
- Wall Segment 13 14
- Wall Segment 14 15
- Wall Segment 15 16
- Wall Segment 16 17
- Wall Segment 17 18
- Wall Segment 18 19
- ----- Wall Segment 19 20. Top
- —— Fluid Temperature. °C

The following topics have been addressed during today's presentation

- Evaluation of vessel and piping wall temperatures using the fundamental heat transfer equation outlined in API Standard 521
- Advantages and characteristics of the wall segmentation approach implemented in SuperChems[™]
- Application of the wall dynamics approach in SuperChems^{TT} via 2 case studies: (1)</sup> evaluation of a pressure vessel, and (2) evaluation of a low-pressure atmospheric tank

Thank you very much! Questions?

About ioMosaic Corporation

Through innovation and dedication to continual improvement, ioMosaic has become a leading provider of integrated process safety and risk management solutions. ioMosaic has expertise in a wide variety of areas, including pressure relief systems design, process safety management, expert litigation support, laboratory services, training, and software development.

ioMosaic offers integrated process safety and risk management services to help you manage and reduce episodic risk. Because when safety, efficiency, and compliance are improved, you can sleep better at night. Our extensive expertise allows us the flexibility, resources, and capabilities to determine what you need to reduce and manage episodic risk, maintain compliance, and prevent injuries and catastrophic incidents.

Our mission is to help you protect your people, plant, stakeholder value, and our planet.

For more information on ioMosaic, please visit: www.ioMosaic.com

